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CMPO和TBP在离子液体中选择性萃取水溶液中铀酰离子的研究

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摘要:研究了以辛基(苯基)-*N*,*N*-二异丁基胺甲酰基甲基氧化膦(CMPO)和磷酸三丁酯(TBP)在离子液体(ILs)中选择性萃取水溶液中的铀酰离子(UO²⁺).离子液体为1-烷基-3-甲基咪唑双三氟甲基磺酰亚胺盐(C_nmimNTf₂, *n*=2,4,6,8).水相硝酸浓度以及离子液体的取代基链长对UO²⁺的分配比和萃取选择性均有影响.与TBP相比,CMPO在离子液体中对UO²⁺具有更高的萃取分配比和更好的萃取选择性.对模拟废液(SLW)萃取发现,Zr⁴⁺,ReO₄和Cs⁺是主要的竞争离子.ReO₄和Cs⁺可被离子液体本身萃取,而Zr⁴⁺则是被CMPO和TBP萃取而不被离子液体本身萃取.本研究工作表明,CMPO-ILs体系在铀酰离子的选择性萃取分离中具有一定的应用前景.

关键词: 离子液体; 萃取; 分离; 选择性; 铀酰离子 中图分类号: O645

Investigation of Selective Extraction of UO₂²⁺ from Aqueous Solution by CMPO and TBP in Ionic Liquids

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Abstract: The selective extraction of UO_2^{2+} from aqueous solution in the presence of other metal ions by octylphenyl-*N*,*N*-diisobutylcarbamoylmethylphosphine oxide (CMPO) and tri-*n*-butyl phosphate (TBP) in ionic liquids (ILs), namely 1-alkyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imides (C_nmimNTf₂, *n*=2, 4, 6, 8), were studied. The influences of the nitric acid concentration and the IL alkyl chain length on the distribution ratio and selectivity were examined. Compared with TBP in C₄mimNTf₂, CMPO in the ILs gave higher distribution ratios and better selectivities. Zr^{4+} , ReO_4^{-} , and Cs^+ were the main competing ions in the separation of UO_2^{2+} from simulated liquid waste (SLM) by the C_nmimNTf₂ systems. ReO_4^{-} and Cs^+ were extracted by the ILs themselves. Zr^{4+} was extracted by CMPO or TBP in the ILs but not by the ILs themselves. This work gives further information on the use of ILs, and provides a basis for matching extractants with ILs in the processing of spent nuclear fuel.

Key Words: Ionic liquid; Extraction; Separation; Selectivity; UO2⁺

1 Introduction

Room temperature ionic liquids (ILs) have been considered as alternative solvents for synthetic, catalytic, electrochemical and separation sciences because of their unique properties such as low vapor pressure, solvating properties, and thermal stability.¹⁻⁴ Especially, they have been considered as next generation diluents as the replacements of volatile organic compounds (VOCs) in the reprocessing of spent nuclear fuel.⁵⁻³⁰ For the current commercial

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process (PUREX process) for recovering uranium and plutonium from spent nuclear fuel using a 30% solution of tri-*n*-butyl phosphate (TBP) in kerosene, there are still some drawbacks including the volatility and flammability of kerosene and the risk of the system becoming critical if the concentration of fissile products becomes too large.²⁰ The utilization of ILs can overcome these drawbacks and help reduce the risk to some extent,³¹ and a number of studies have been performed.

The extraction of uranium using ILs as solvents has been performed with TBP as the extractant.¹⁵⁻²¹ The extraction of UO₂²⁺ from nitric acid medium by 1.1 mol·dm⁻³ of TBP in the ILs 1butyl-3-methylimidazolium hexafluorophosphate (C4mimPF6) and bis(trifluoromethylsulfonyl)imides (C4mimNTf2) was reported by Rao and coworkers.¹⁵⁻¹⁷ The effect of the concentration of nitric acid on the distribution ratio differs greatly depending upon the nature of the anion of an IL used as diluent. Dietz and Stepinski¹⁸ studied the anion concentration-dependent partitioning mechanism in the extraction of UO_2^{2+} into the ILs C_nmimNTf₂ (n=5, 8, 10). The mode of partitioning of UO_2^{2+} between nitrate-containing aqueous phase and the ILs (C₅mimNTf₂ and C₈mimNTf₂) in the presence of TBP was shown to change from a cation-exchange process to one involving the extraction of a neutral complex UO₂(TBP)₂(NO₃)₂ as the concentration of nitrate was increased. In C10mimNTf2 system, the neutral complex extraction was the predominant mode of partitioning, regardless of the nitrate concentration.¹⁸ Billard et al.¹⁹ studied the extraction mechanism in the extraction of UO_2^{2+} by TBP in C₄mimNTf₂, where the uranyl extraction is shown to proceed via a double cationic exchange at low acidities and via an anionic exchange at high acidity, excluding the extraction of the usual UO₂(NO₃)₂(TBP)₂ neutral species evidenced in dodecane. Bell and Ikeda²⁰ used ammonium based hydrophobic ILs in the liquid-liquid extraction of UO_2^{2+} from the aqueous solution of nitric acid by TBP and found that cation-exchange, anion-exchange, and the partitioning of a neutral complex were involved depending on the concentration of nitric acid and the hydrophobicity of the IL used.

The extraction mechanism is more complicated in TBP-IL system than that in TBP-kerosene system. This difference may influence the selectivity of TBP to uranyl ion. For the complicated components of spent nuclear fuel, selective extraction of $UO_2^{2^+}$ from aqueous solution containing other fission products must be considered when an IL instead of kerosene acts as diluent. However, there are no reports on the separation of $UO_2^{2^+}$ from aqueous phase in the presence of other metal ions by TBP in ILs.

Furthermore, although TBP is a very excellent extractant in the present commercial process using kerosene as diluent, it must not be the case in the IL system. Actually, some other extractants, such as octyl-phenyl-N,N-diisobutylcarbamoylmethylphosphine oxide (CMPO), bis(2-ethylhexyl)phosphate acid (HDEHP), and task specific ILs bearing phosphoryl groups, have been used in the IL system for extracting UO_2^{2+} .^{14,32–35} For example, Visser *et al.*³² studied the extraction of UO_2^{2+} by CMPO and TBP in C₄mimPF₆ and C₈mimNTf₂, and investigated the coordination environment

of uranyl ion in ILs by extended X-ray absorption fine structure (EXAFS) measurements. The utilization of other extractants instead of TBP in ILs also needs the examination of their selectivities to $UO_2^{2^+}$ in the presence of other metal ions.

The extraction selectivity toward $UO_2^{2^+}$ is of great importance for the recycling uranium in the reprocessing of the spent nuclear fuel. Especially, research should be focused on the extraction performance of $UO_2^{2^+}$ in the presence of other metal ions and the discovery of the competing ions. The extraction of $UO_2^{2^+}$ by TBP and CMPO in ILs have been studied in the literature,³² but their extraction selectivity toward $UO_2^{2^+}$ has not yet been investigated. Thus, in this work, we mainly focused our attention on the selective extraction of $UO_2^{2^+}$ from aqueous phase in the presence of other metal ions, using CMPO and TBP as the extractants in the ILs C_nmimNTf₂.

2 Experimental

2.1 Materials

C_nmimNTf₂ (*n*=2, 4, 6, 8) were synthesized *via* metathetical reaction from C_nmimBr and LiNTf₂,³⁶ and the purity was over 99% as detected by NMR and elemental analysis. Both C_nmimBr and LiNTf₂ (AR) were purchased from Lanzhou Institute of Chemical Physics, China. CMPO (97%) was purchased from Strem Chemicals Inc., USA. TBP (AR) was purchased from Sinopharm Chemical Reagent Co., Ltd., China. Sr(NO₃)₂, CsNO₃, ZrOCl₂ · 8H₂O, Cr(NO₃)₃ · 9H₂O, and Ni(NO₃)₂ · 6H₂O were all of analytical grade. NH₄ReO₄ (≥99%) was purchased from Sigma-Aldrich. Ru(NO)(NO₃)₃ (1.5% Ru *w*/*v* (g · mL⁻¹) solution in water) was purchased from J&K Scientific Ltd., China. Nd(NO₃)₃ · *m*H₂O (*m*≈ 6, ≥99%) was purchased from Sinopharm Chemical Reagent Co., Ltd., China. UO₂(NO₃)₂ · 6H₂O (≥98.5%) was obtained from INET, Tsinghua University, China. All other chemicals were of analytical grade.

2.2 Methods

2.2.1 Preparation of simulated liquid waste

According to the literature,³⁷ Sr, Cs, Cr, Ni, Nd, and U are all the components of the liquid waste generated from the pressurized heavy water reactor (PHWR). On the other hand, Sr, Cs, Zr, Tc, Ru, Nd, and U are all the components of the pressured water reactor (PWR) fuel.³⁸ In this work, Sr, Cs, Zr, Cr, Re, Ru, Ni, Nd, and U were contained in the simulated liquid waste (SLW), in which Re was used as surrogate of Tc. To save uranyl nitrate consumption, two stock solutions were prepared respectively in the preparation of the SLW. One is the stock solution containing Sr, Cs, Zr, Cr, Re, Ru, Ni, and Nd, prepared by directly dissolving the salts in water. The pH of the stock solution is 1.20. Another is the stock solution of uranyl nitrate (pH=2.72). Then the two stock solutions were mixed, and an appropriate amount of nitric acid was added. To detect the concentrations of all the metal ions by inductively coupled plasma-atomic emission spectrometer (ICP-AES, Leeman, USA) as accurately as possible, the concentrations of the metal ions in the SLW have been modified and they are

Table 1	Concentrations of metal ions in the simulated liquid
	waste (SLW) used in this work

Element	Concentration/(g·dm ⁻³)	
Sr	0.54	
Cs	0.54	
Zr	0.68	
Cr	0.34	
Re	0.15	
Ru	0.38	
Ni	0.17	
Nd	1.00	
U	2.38	

The concentration of the adding HNO3 varies from 0 to 4 mol $\cdot\,dm^{\text{-3}}.$

listed in Table 1.

2.2.2 Extraction studies

In each extraction experiment, 0.5 mL of C_nmimNTf₂ containing CMPO or TBP and 0.5 mL of aqueous solution containing metal ions were slowly added by a transfer liquid gun (Eppendorf) into a plastic centrifuge tube, followed by vibrating for 24 h at 298.2 K. Actually, we performed the kinetic experiments and found that the equilibration time was about 1 and 6 h for the extraction of UO2²⁺ by 1.1 mol·dm⁻³ of TBP in C₄mimNTf₂ and 0.02 mol·dm⁻³ of CMPO in C_n mimNTf₂ (n=4, 8), respectively. However, we previously found that the equilibration time was about 16 h for the extraction of Cs⁺ by C₄mimNTf₂ only. The equilibration time for the extraction of Zr⁴⁺ and ReO₄⁻ by IL systems was both less than 1 h. Because Cs⁺ was one of the metal ions in the SLW, we performed all the extraction experiments with vibrating time of 24 h in this work. After vibrating, the mixture was centrifuged for 2 min at 10000 $r \cdot min^{-1}$ and the two phases were separated. The concentrations of metal ions remained in the aqueous phase were analyzed by ICP-AES with the uncertainty within 5%. The distribution ratio (D) was calculated as

$$D = \frac{C_{\rm i} - C_{\rm f}}{C_{\rm f}} \tag{1}$$

where C_i and C_f designate the initial and final concentrations of metal ions in the aqueous phase, respectively.

3 Results and discussion

3.1 Extraction of UO₂²⁺ by CMPO in ILs

Fig.1 shows the results of the extraction by CMPO in $C_n \text{mimNTf}_2$ (*n*=2, 4, 6, 8) from the aqueous solution of uranyl nitrate with near zero free acidity ("with near zero free acidity" means the aqueous solution without the addition of HNO₃, and the pH of the aqueous solution is about 3.10 at 298.2 K). Increase in the concentration of CMPO leads to high distribution ratio of UO_2^2 ⁺. Among the selected ILs $C_n \text{mimNTf}_2$ (*n*=2, 4, 6, 8), $C_2 \text{mimNTf}_2$ system has the highest distribution ratio toward $UO_2^{2^+}$. Lengthening the alkyl chain of ILs decreases the distribution ratio.

The effect of nitric acid on the extraction of $UO_2^{2^+}$ by 0.02 mol· dm⁻³ of CMPO in C_nmimNTf₂ (*n*=2, 4, 6, 8) is shown in Fig.2. The distribution ratio in the CMPO-C₂mimNTf₂ system shows a very little variation as the concentration of the adding HNO₃ (C_{HNO3})



Fig.1 Dependence of the distribution ratio of $UO_2^{2+}(D_u)$ from the aqueous solutions with near zero free acidity on the concentration of CMPO in the ILs $C_u mimNTf_2$ (*n*=2, 4, 6, 8)

The initial concentration of UO_2^{2+} in the aqueous phase is 0.01 mol·dm⁻³.

varies from 0 to 4 mol·dm⁻³. For the system using an IL with long alkyl chain on the imidazolium cation, e.g., C_8 mimNTf₂, adding nitric acid induces an obvious increase in the distribution ratio. Lengthening the alkyl chain leads to a decrease in the distribution ratio at $C_{HNO_3}=0$ mol·dm⁻³ and an increase in the distribution ratio at 4 mol·dm⁻³ of HNO₃. The difference of the extraction behavior of CMPO in different ILs is very likely due to the difference in the extraction mechanism, i.e., the different proportions between the cation exchange, the anion exchange, and the neutral complex extraction.^{18–20,39}

Previous studies of the extraction of $UO_2^{2^+}$ by TBP-C₄mimNTf₂ showed that the distribution ratio varied significantly upon the addition of nitric acid.¹⁶⁻¹⁸ For comparison, we also performed the extraction of $UO_2^{2^+}$ by 1.1 mol·dm⁻³ of TBP in C₄mimNTf₂ as C_{HNO3} varied from 0 to 4 mol·dm⁻³, and the result is also shown in Fig.2. TBP-C₄mimNTf₂ can efficiently extract $UO_2^{2^+}$ with a distribution ratio of 4.6 from the aqueous solution with near zero free acidity. The distribution ratio of $UO_2^{2^+}$ decreases upon the addition of nitric





The initial concentration of UO_2^{2+} in the aqueous phase is 0.01 mol·dm⁻³.

acid and reaches the lowest value of 0.38 at 0.5 mol \cdot dm⁻³ of HNO₃, and then increases upon continuous addition of HNO₃, which is consistent with the tendency reported in the literature.¹⁶⁻¹⁸

3.2 Selective extraction of UO₂²⁺ from SLW

In the reprocessing of the spent nuclear waste, the composition of the liquid waste is very complicated. There are many kinds of metal ions in the liquid waste. The selective extraction of $UO_2^{2^+}$ from the SLW by the IL systems was detected in the present work. Among the metal ions in the SLW, Cs^+ and Sr^{2^+} are the major radioactive fission products in the spent nuclear waste, contributes a large part of the heat load and radiation. ReO_4^- is used as the surrogate for TcO_4^- , which is one of the main fission products of uranium. Nd^{3^+} is a representative of the lanthanides and minor actinides.

Detection of the extraction of the SLW by 1.1 mol · dm⁻³ of TBP, 0.02 mol·dm⁻³ of CMPO in C₄mimNTf₂, and 0.02 mol·dm⁻³ of CMPO in C₈mimNTf₂ shows that only UO₂²⁺, Zr⁴⁺, ReO₄⁻, and Cs⁺ in the SLW are extracted while other metal ions are not extracted. Fig.3 shows the distribution ratios of UO₂²⁺, Zr⁴⁺, ReO₄⁻, and Cs^+ depending on C_{HNO_3} . For clarity, the distribution ratios of the metal ions which are not extracted are not presented in the figures. It was noticed that the distribution ratio of UO_2^{2+} by TBP in C₄mimNTf₂ at C_{HNO_3} =0.5 mol·dm⁻³ in Fig.3(a) is higher than that in Fig.2. This is because the concentration of NO₃ is about 0.1 mol \cdot dm⁻³ in the SLW without the addition of HNO₃, which influences the extraction of $UO_2^{2^+}$. Zr⁴⁺ is extracted at C_{HNO_3} over 2 mol · dm⁻³ and its distribution ratio increases with the increase in the concentration of HNO₃. Cs⁺ and ReO₄⁻ are extracted at all HNO₃ concentrations. In general, CMPO-C₄mimNTf₂ system behaves better than CMPO-C8mimNTf2 system in the selective extraction of UO2²⁺ from the SLW, and CMPO in C₄mimNTf₂ shows a relatively good selectivity towards UO_2^{2+} , as compared with TBP in C₄mimNTf₂.

We also studied the extraction of the SLW by 0.04 mol·dm⁻³ of CMPO in C₄mimNTf₂ and the result is shown in Fig.4. The distribution ratio of UO₂²⁺ is enhanced dramatically and almost all the UO₂²⁺ ions in the SLW are extracted into the IL phase. Simultaneously, the distribution ratio of Zr⁴⁺ is increased and Nd³⁺ is extracted. Different from the extraction of the SLW by 0.02 mol·dm⁻³ of CMPO in ILs, Zr⁴⁺ is extracted at low $C_{\text{HNO}3}$. The distribution ratio of Nd³⁺ decreases as HNO₃ is added. This result suggests that the concentration of the extractant in ILs should be fixed carefully if CMPO is utilized in the practical application.

3.3 Extraction of SLW by IL only

We detected the extraction of the SLW by C₄mimNTf₂ and C₈mimNTf₂, and the results are shown in Fig.5. One can see that ReO₄⁻ and Cs⁺ are extracted by the IL in the absence of extractants. The distribution ratio of Cs⁺ is close to that in the systems with extractants. Our group²⁵ previously reported that C_nmimNTf₂ can extract Cs⁺ from aqueous solution *via* cation exchange. A further study suggested that the coordination of the anion NTf₂⁻ to Cs⁺ accounts for the extraction.⁴⁰ The extraction ability of C_nmimNTf₂ to Cs⁺ induces high distribution ratio during the extraction of Cs⁺



Fig.3 Distribution ratio of metal ions depending on the concentration of the adding HNO₃ in the extraction of SLW by (a) 1.1 mol·dm⁻³ of TBP in C₄mimNTf₂, (b) 0.02 mol·dm⁻³ of CMPO in C₄mimNTf₂, and (c) 0.02 mol·dm⁻³ of CMPO in C₈mimNTf₂ Other metal ions in the SLW are not extracted.

from aqueous solution, but it leads to an undesirable problem in the selective extraction of UO_2^{2+} . Especially, the competing extraction of Cs^+ is hard to be reduced by varying the concentration of HNO₃.

The extraction of ReO₄ by C₄mimNTf₂ and C₈mimNTf₂ results from the anion exchange, according to the literature.²⁴ However, one can see that the distribution ratios of ReO₄ in Fig.5 is much lower than those in Fig.3 and Fig.4. It was reported that TcO₄ acts as the counterion in the extraction of $UO_2^{2^+}$.⁴¹ On the other hand, Chaumont *et al.*⁴² studied the complexation of ReO₄ and $UO_2^{2^+}$ in



Fig.4 Distribution ratio of metal ions depending on the concentration of the adding HNO₃ in the extraction of SLW by 0.04 mol·dm⁻³ of CMPO in C₄mimNTf₂ Other metal ions in the SLW are not extracted.

aqueous solution, acetonitrile, C₄mimNTf₂ and other two ILs. They found that ReO₄⁻ behaves as a weak ligand in aqueous solution and as a strong ligand in acetonitrile and in the ILs.⁴² Thus the higher distribution ratio of ReO₄⁻ as UO₂²⁺ was extracted could be attributed to the counterion effect, i.e., the interaction of ReO₄⁻ with UO₂²⁺. Furthermore, if we relook the distribution ratio of ReO₄⁻ in Fig.6, we can infer that the extractant also influences the



Fig.5 Distribution ratio of metal ions depending on the concentration of the adding HNO₃ in the extraction of SLW by (a) C₄mimNTf₂ only and (b) C₈mimNTf₂ only Other metal ions in the SLW are not extracted.

interaction between ReO_4^- and UO_2^{2+} in ILs, thus the distribution ratios of ReO_4^- are different in the extraction of the SLW by TBP-C₄mimNTf₂ and CMPO-C₄mimNTf₂ systems.

3.4 Extraction of Zr⁴⁺ by IL systems

The above results indicate that Zr^{4+} , ReO_4^- , and Cs^+ are the main competing ions in the separation of UO_2^{2+} from the SLW by the $C_nmimNTf_2$ systems, and Nd^{3+} is extracted at high CMPO concentration. Compared the results in Fig.3 and Fig.4, one can see that Nd^{3+} is only extracted at high CMPO concentration. This is because CMPO in $C_4mimNTf_2$ can extract the lanthanide ions with a high distribution ratio according to the literature,⁴³ and the extraction of Nd^{3+} is restrained in the presence of UO_2^{2+} .

The results in Fig.5 indicate that no Zr^{4+} is extracted by $C_n \text{mimNTf}_2$. Actually, the extraction of Zr^{4+} is attributed to the presence of CMPO or TBP. As shown in Fig.6, CMPO in ILs can extract Zr^{4+} , and the distribution ratio increases with the increase in $C_{\text{HNO}3}$. The distribution ratio of Zr^{4+} in C₄mimNTf₂ system is lower than that in C₈mimNTf₂ system at high $C_{\text{HNO}3}$, consisting with the result in the extract Zr^{4+} in C₄mimNTf₂ at $C_{\text{HNO}3}$ lower than 2 mol·dm⁻³.

3.5 Extraction of the SLW by TBP in dodecane

For comparison, the extraction of the SLW by 1.1 mol·dm⁻³ of TBP in dodecane has been performed and the result is shown in Fig.7. In the dodecane system, the distribution ratio of UO_2^{2+} increases with the increase in C_{HNO_3} . Zr⁴⁺ is not extracted at C_{HNO_3} lower than 2 mol·dm⁻³, similar to that in the TBP-C₄mimNTf₂ system. Compared with the TBP-dodecane system, one can see that one of the advantages to use ILs as solvents is that Ru(III) is not extracted by the IL systems. Because of the complicated complexes of nitrosylruthenium,⁴⁴ more research is required in the future to figure out why the dodecane system can but the IL systems cannot extract Ru(III). On the other hand, a disadvantage in the IL systems is that the IL itself is able to extract Cs⁺ despite the variation of HNO₃ concentration, although the distribution ratio of Cs⁺ can be decreased with the increase in the alkyl length of the IL cations.



Fig.6 Distribution ratio of Zr⁴⁺ depending on the concentration of the adding HNO₃ by 0.02 mol·dm⁻³ of CMPO in C_nmimNTf₂ (*n*=4, 8) and by 1.1 mol·dm⁻³ of TBP in C₄mimNTf₂



Fig.7 Distribution ratio of metal ions depending on the concentration of the adding HNO₃ in the extraction of SLW by 1.1 mol·dm⁻³ of TBP in dodecane Other metal ions in the SLW are not extracted.

The above results suggest that TBP and CMPO in ILs can selectively extract UO_2^{2+} from the SLW, and Zr^{4+} , ReO₄⁻, Cs⁺ are the main competing ions. Compared with TBP, CMPO may be a better candidate for the application of ILs in the separation of UO_2^{2+} in the reprocessing of spent nuclear fuel. However, this work is a very preliminary study, for the composition of the spent nuclear waste is much more complicated than that of the SLW employed in this work. To evaluate the IL-based extraction system as a promising strategy in the reprocessing of spent nuclear waste, a great deal of work will be required in the future.

4 Conclusions

 $UO_2^{2^+}$ can be selectively extracted by TBP or CMPO in imidazolium based ILs from aqueous solution in the presence of other metal ions. Among the selected metal ions, Zr^{4^+} , ReO_4^- , and Cs^+ are the main competing ions. CMPO performs a better selectivity to $UO_2^{2^+}$ than TBP does. Both the extraction capacity and selectivity of CMPO in ILs vary as the alkyl chain of C_n mimNTf₂ lengthens. CMPO-C₄mimNTf₂ may be a candidate for the application of ILs in the separation of $UO_2^{2^+}$ in the reprocessing of spent nuclear fuel. This work will be helpful for the practical application of IL-based extraction system in the reprocessing of spent nuclear fuel.

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